

Communication Engineer

Satcom ABC series (4)



WU Boyang
APMT

Communication Payload

Parameters

Carrier Assignment

Link Budget

Frequency Resource and RF Equipments

Payload Management

Spectrum Assignment

Carrier Management

Technical Support

Marketing Support

Costumer Support

Sun Outage

Frequency Coordination

❖ Transponder

- Combination of receiver, frequency converter and transmitter
- Main parameters
 - ⇒ G/T, SFD and EIRP
 - ⇒ relative to antenna pattern (geographical location)
 - ⇒ relative to operation frequency (transponder number)
 - ⇒ city tables and isograms
- G/T and SFD
 - ⇒ showing transponder Rx performance at its service area
 - ⇒ depending on antenna Rx gain pattern
- EIRP
 - ⇒ showing transponder Tx power at its service area
 - ⇒ depending on antenna Tx gain pattern

❖ figure of merit

- Characterization of receive system performance

$$G/T \text{ (dB/k)} = G \text{ (dBi)} - T_{\text{SYS}} \text{ (dBk)}$$

where, G is antenna gain and T_{SYS} is equivalent noise temperature of receiving system

$$T_{\text{SYS}} = T_{\text{ANT}} + T_{\text{RCV}}$$

- T_{ANT} : antenna noise temperature

⇒ depends on its gain pattern with the thermal environment

⇒ night sky: roughly 4 Kelvin

⇒ earth ground: physical temperature

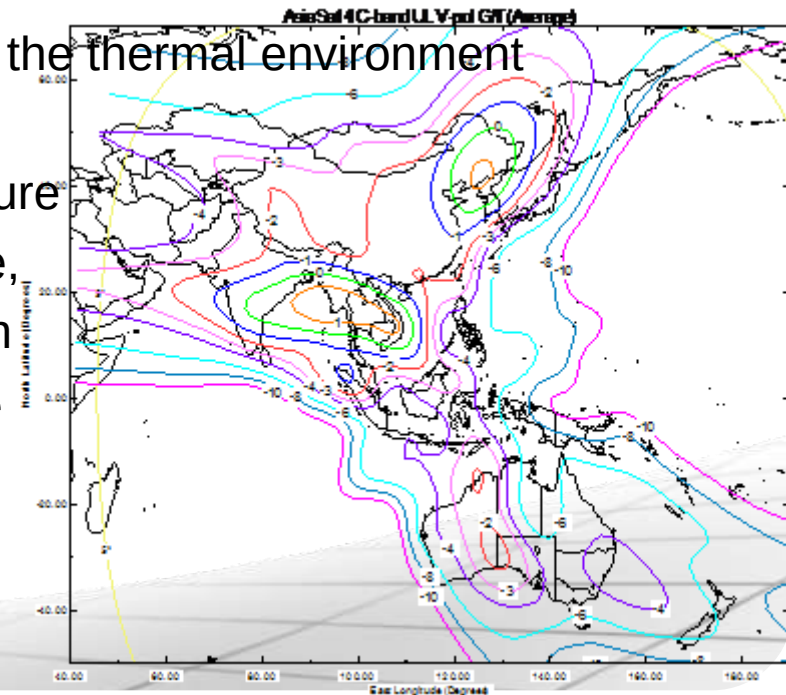
⇒ sun surface: when in sun outage, too high to interrupt transmission

- T_{RCV} : receiver noise temperature

- G/T at beam peak

⇒ C-band: about 1 dB/k

⇒ Ku-band: about 7dB/k



❖ Saturated Flux Density

- Flux density at receive antenna required to saturate HPA

$$\text{SFD} = C + \text{Attn} - G/T \text{ (dBW/m}^2\text{)}$$

where C is a constant (-90 to -100), Attn is corresponding channel gain step (0 to 20 even to 30)

⇒ normal range: -70 to -100 dBW/m²

⇒ normally selected value: -85 to -93 dBW/m²

- More sensitive SFD, less uplink power required

⇒ less C/N and C/I

- SFD listed in data table is usually relative to a specified Attn

⇒ 0dB Attn (most sensitive SFD) or 8dB Attn (normally used SFD)

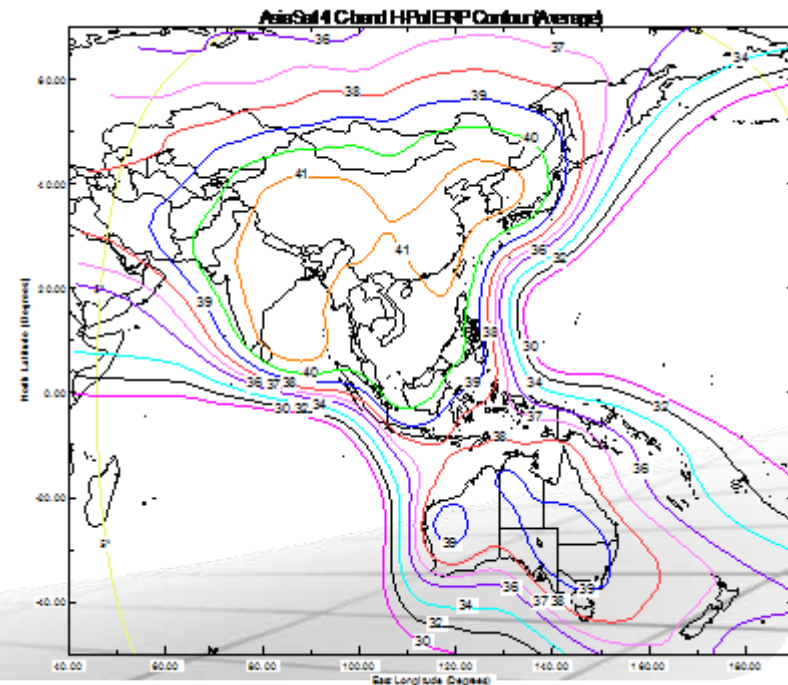
❖ EIRP

- Effective Isotropic Radiated Power
- The power radiated by a directional antenna with an antenna gain relative to an isotropic antenna

$$\text{EIRP (dBW)} = P \text{ (dBW)} - \text{Loss (dB)} + G \text{ (dBi)}$$

where, P is HPA output power, Loss is wave guide loss between HPA and antenna feed, G is antenna gain

- EIRP at beam peak
 - ⇒ C-band: about 41 dBW
 - ⇒ Ku-band: about 56 dBW



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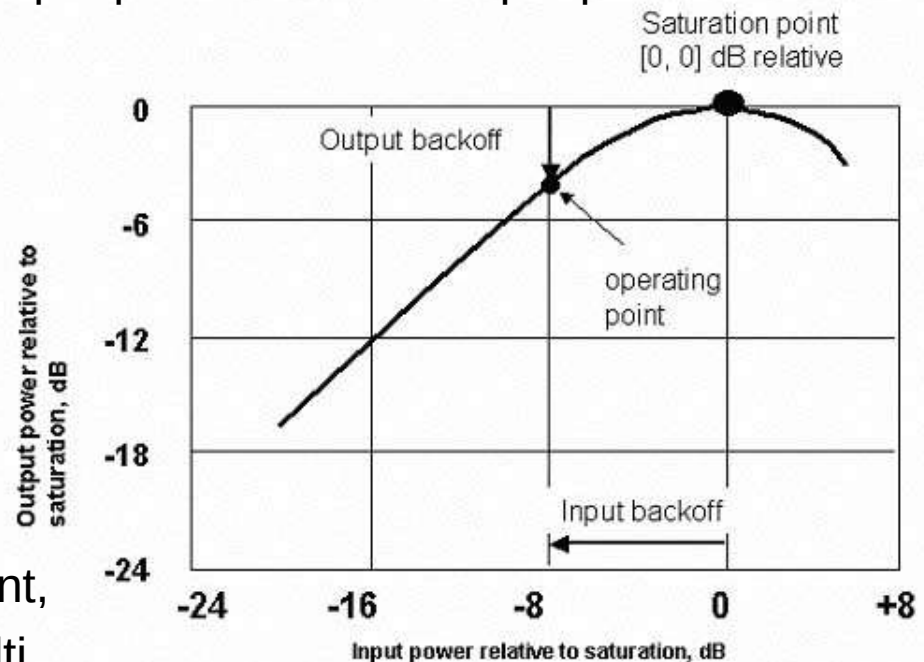
Frequency Coordination

❖ TWTA

- HPA of satellite transponder: non-linear amplifier
- Output/Input relationship: gain transfer curve
 - ⇒ relationship between output power level and input power level

❖ Gain transfer curve

- Y-axis: output power
- X-axis: input power
- Saturation point
 - ⇒ vertex of the curve
 - ⇒ reference point
- Linearity range
 - ⇒ closer to saturation point, higher efficiency at multi carrier usage



❖ Back-off

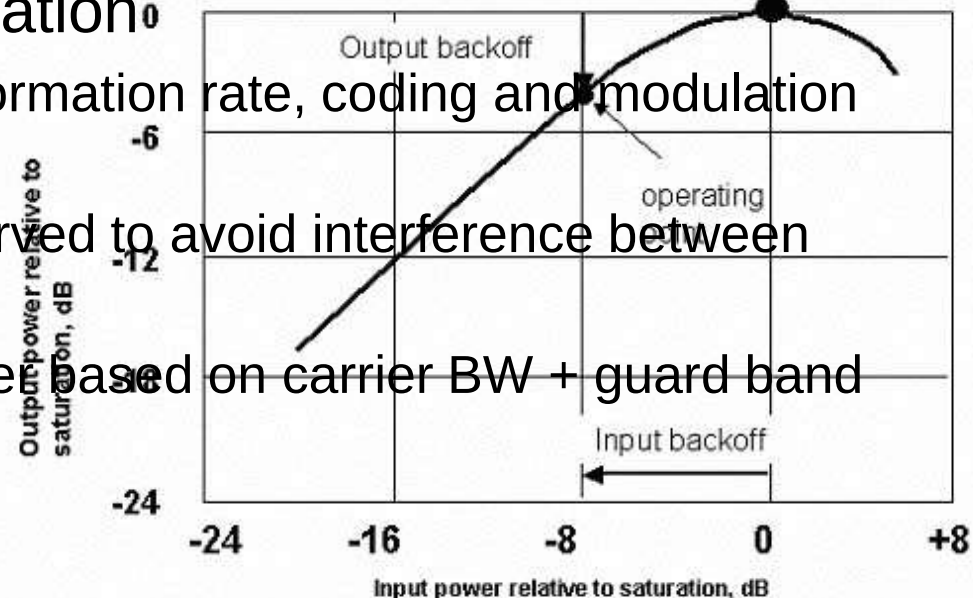
- Input back-off: difference of input power level between operating point and saturation point
- output back-off: difference of output power level between operating point and saturation point
- Linear back-off: Operation point at highest linearity range to avoid IM

⇒ for LCTWTA: 3dB output back-off / 6dB input back-off

Saturation point
[0, 0] dB relative

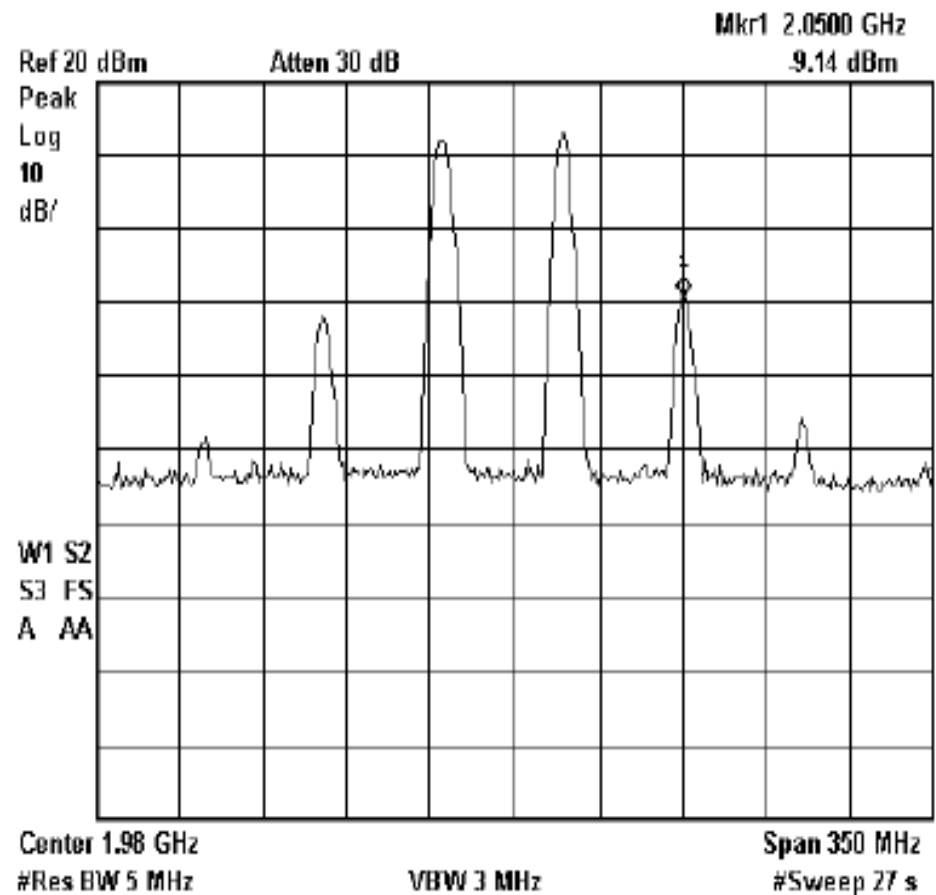
❖ Carrier bandwidth allocation

- Calculated by signal information rate, coding and modulation type
- Proper guard band reserved to avoid interference between adjacent carriers
- Rental for the user carrier based on carrier BW + guard band



Intermodulation

- ❖ Intermodulation component
- ❖ Occurred at multi carrier operation
 - Interfered to other carriers



❖ Transponder operation point

- Reserving sufficient output back-off
- To keep transponder power limited in linear range

❖ Carrier power allocation

- Transponder resource: power and bandwidth
- When power balanced with bandwidth

$$\text{EIRP}_C = \text{EIRP}_{xpd} - \text{OPBO}_C$$

where, EIRP_C and EIRP_{xpd} means EIRP for carrier and transponder, and OPBO_C means carrier output back-off

- Downlink carrier power allocated as

$$\text{OPBO}_C = \text{OPBO}_{xpd} + 10 \lg(\text{BW}_{xpd}/\text{BW}_C)$$

where, OPBO_C and OPBO_{xpd} means output back-off of carrier and transponder respectively, and BW_{xpd} and BW_C means bandwidth of transponder and carrier

- If customer deserves higher carrier power than average power of the transponder, the payment should be more than average

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Frequency Coordination

❖ Target

- To calculate antenna elevation and azimuth angle
- To calculate carrier power and bandwidth
- To estimate up-link C/N, down-link C/N and total C/N (interference involved or not), and link margin

❖ Input data

- Transponder parameters
 - ⇒ G/T at up-link site
 - ⇒ SFD at up-link site (corrected by gain step setting)
 - ⇒ EIRP at down-link site
 - ⇒ Up-link frequency of the carrier (down-link frequency may be auto-calculated by preset transfer frequency)
 - ⇒ Output back-off (input back-off may be auto-calculated by preset gain transfer data)

❖ Input data (cont.)

➤ Carrier information

- ⇒ information rate
- ⇒ modulation type
- ⇒ coding rate
- ⇒ required E_b/N_0 (energy per bit to noise power density ratio, relative to modulation type, coding rate and bit error rate)

➤ Parameters for up-link and down-link earth stations

- ⇒ location with longitude and latitude
- ⇒ antenna size, antenna efficiency, and system noise temperature

➤ Parameters for fade and interference

- ⇒ pointing error, atmospheric absorption, troposphere fading, rain attenuation
- ⇒ C/T (carrier to noise temperature ratio) about adjacent satellites, intermodulation, and cross polarization interference

❖ Data correction

- Estimated results need to be manually revised one or more times
- Data need to be revised before calculation
 - ⇒ allocated bandwidth (auto-calculated occupied bandwidth + proper guard band)
 - ⇒ suggested HPA output power ($>$ calculated up-link power + back-off value, and match product standard)
- Data need to be revised after first round of calculation
 - ⇒ carrier back-off (if calculated system margin is too high or too low)
 - ⇒ modulation type and/or coding rate (if calculated system margin is too high or too low)
 - ⇒ U/L antenna size (if calculated HPA output power is too high)
 - ⇒ D/L antenna size (if calculated system margin is not enough)

❖ Sequence for link budget calculation

- Multi input, and multi output estimation
 - ⇒ all output data may be revised by any input data correction
 - ⇒ several calculation sequences could be used
- Carrier priority: preset carrier with changeable Rx antenna
 - ⇒ according to desired carrier modulation type and coding rate, using balanced or augmented back-off, selecting proper receive antenna size, to meet the required margin
- Aperture priority: preset Rx antenna with changeable carrier
 - ⇒ according to desired receive antenna size, using balanced or augmented back-off, selecting proper carrier modulation type and coding rate, to meet the required margin
- Back-off adjustment
 - ⇒ bandwidth limited result: $P\% < BW\%$, usable power wasted
 - ⇒ power limited result: $P\% > BW\%$, should pay more for rent
 - ⇒ balanced result: $P\% = BW\%$, power and BW resource fully used

Data and Formulas for Link Budget

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❖ Symbol rate

$$\text{symbol rate} = \text{data rate} / m / \text{CRv} / \text{CRrs}$$

where,

m (modulation index), 1 for BPSK, 2 for QPSK, 3 for 8PSK, and 4 for 16QAM;

CRv (Viterbi coding rate), normally as 7/8, 5/6, 3/4, or 1/2;

CRrs (Reed-Solomon coding rate), normally as 188/204

❖ Carrier bandwidth

$$\text{noise BW (3dB BW)} = \text{symbol rate} \times 1.2$$

$$\text{occupied BW (20BW)} = \text{symbol rate} \times 1.4$$

$$40\text{dB BW} = \text{noise BW} \times 1.4 = \text{symbol rate} \times 1.7$$

➤ Common value of roll-off factor is 1.3

⇒ normally between 1.25 and 1.5

Data and Formula for Link Budget

(cont.)

❖ Antenna gain

- Calculated by aperture and frequency

$$G = 10 \lg (\eta (\pi D / \lambda)^2)$$

where,

η (antenna efficiency), normally valued as 55 to 65 %;

D , aperture of antenna;

λ , wave length relative to carrier frequency

- Estimated by beam width

$$G_{\text{ANT}} = 31000 / (\theta_{\text{Az3dB}} \theta_{\text{El3dB}})$$

where, θ_{Az3dB} and θ_{El3dB} are half power beam widths at azimuth and elevation respectively

- Antenna beam width

$$\text{beamwidth}_{3\text{dB}} = 70 \lambda / D$$

Data and Formula for Link Budget (cont.)

❖ Noise figure

$$N_F = 10 \lg(1 + T/290)$$

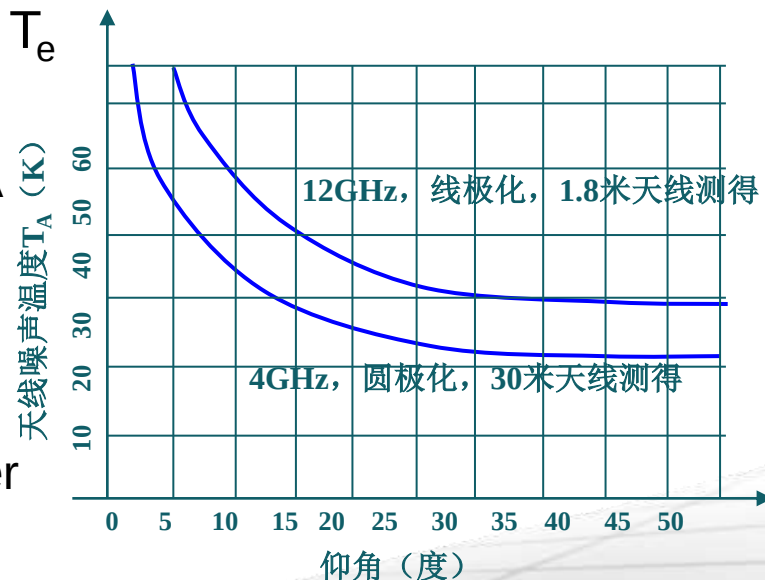
where, T is noise temperature, and 290k is room temperature

- Normally 0.4dB (25-30k) for C-band LNB
- Normally 0.8dB (59k) for Ku-band LNB

❖ Receive system noise temperature

$$T_S \text{ (dBk)} = T_a + (L_F - 1) T_1 + L_F \times T_e$$

where, T_a and T_e are noise temperatures of antenna and LNA respectively, L_F is insertion loss between antenna feed and LNA input, and T_1 is the environment temperature of feeder line



天线噪声温度 (晴朗天气)

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Orbit and Frequency Resource

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❖ Valuable resource

- Expanding requirement against limited resource
- 2 or 2.5 degrees orbital separation for C- and Ku-band
- Early occupation, higher priority
- AP30B resource reserved for developing countries at unpopular frequency

❖ Frequency band

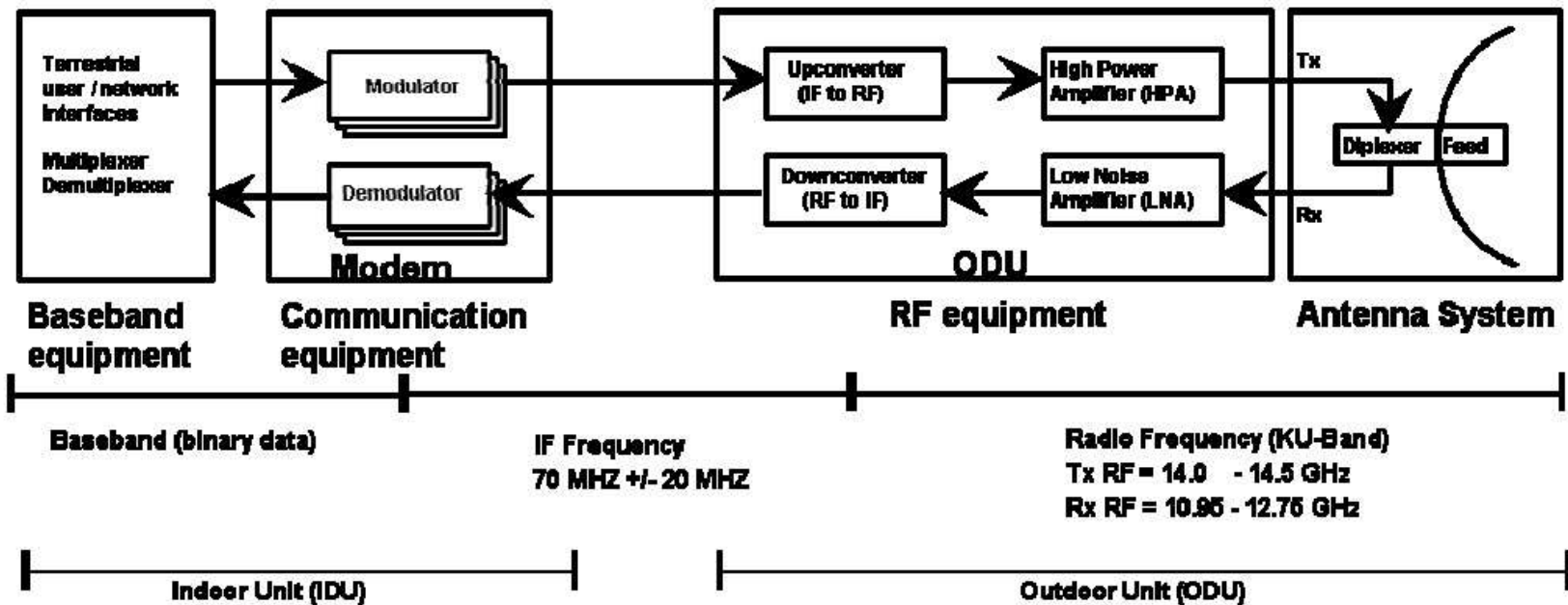
- Standard C-band
 - ⇒ 5925 to 6425 MHz / 3700 to 4200 MHz, $\Delta f = 2225\text{MHz}$
- Standard Ku-band
 - ⇒ 14.0 to 14.5 GHz / 12.25 to 12.75 GHz, $\Delta f = 1.75\text{GHz}$

Block Diagram for Earth Station

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❖ IF connection

- Cable between IDU and ODU at IF band (70MHz or 140MHz)
- RF and Δf of U/C and D/C lied on frequency plan of designated satellite
- Operation frequency band of antenna, HPA, LNA also lied on satellite frequency plan



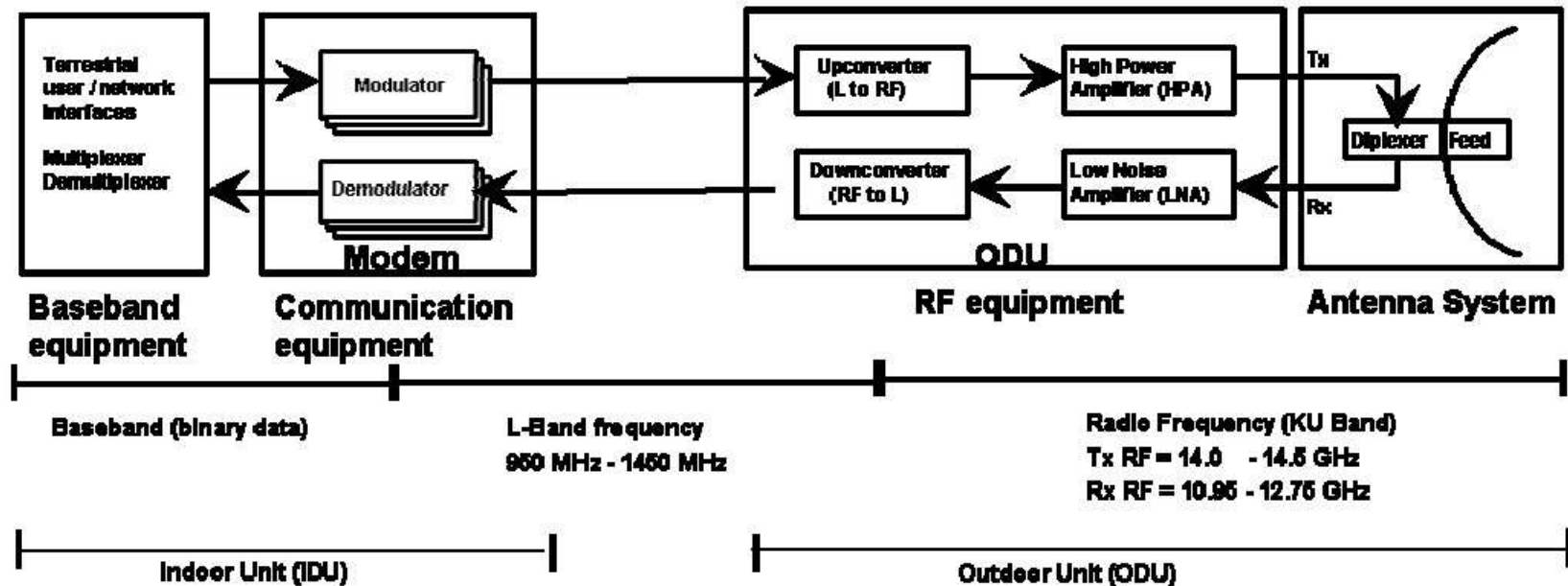
Schematic diagram typical VSAT system with IF radio input

Block Diagram for Earth Station (cont.)

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❖ L-band connection

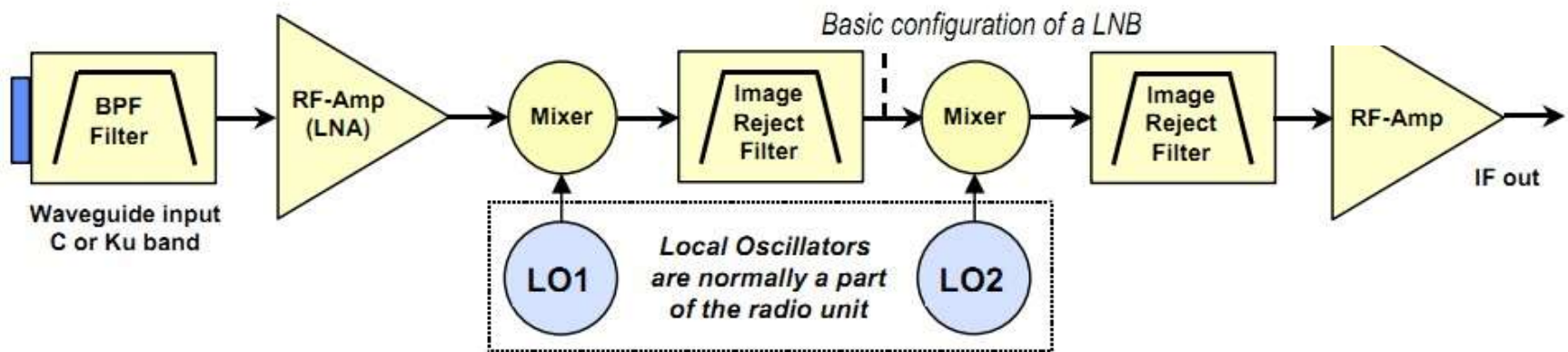
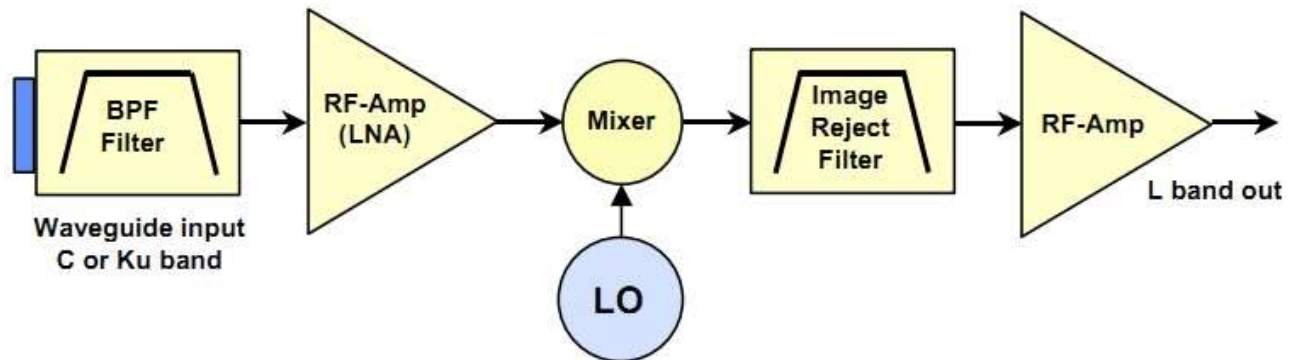
- Cable between IDU and ODU at L-band
- RF and Δf of U/C and D/C lied on frequency plan of designated satellite
- Operation frequency band of antenna, HPA, LNA also lied on satellite frequency plan



Schematic diagram typical VSAT system with L band radio input

Low Noise Amplifiers

- ❖ LNA: only amplifier (50 to 100 dB gain)
- ❖ LNB: amplifier with D/C, output at L-band
- ❖ LNC: amplifier with D/Cs, output at IF, (80-100 dB)



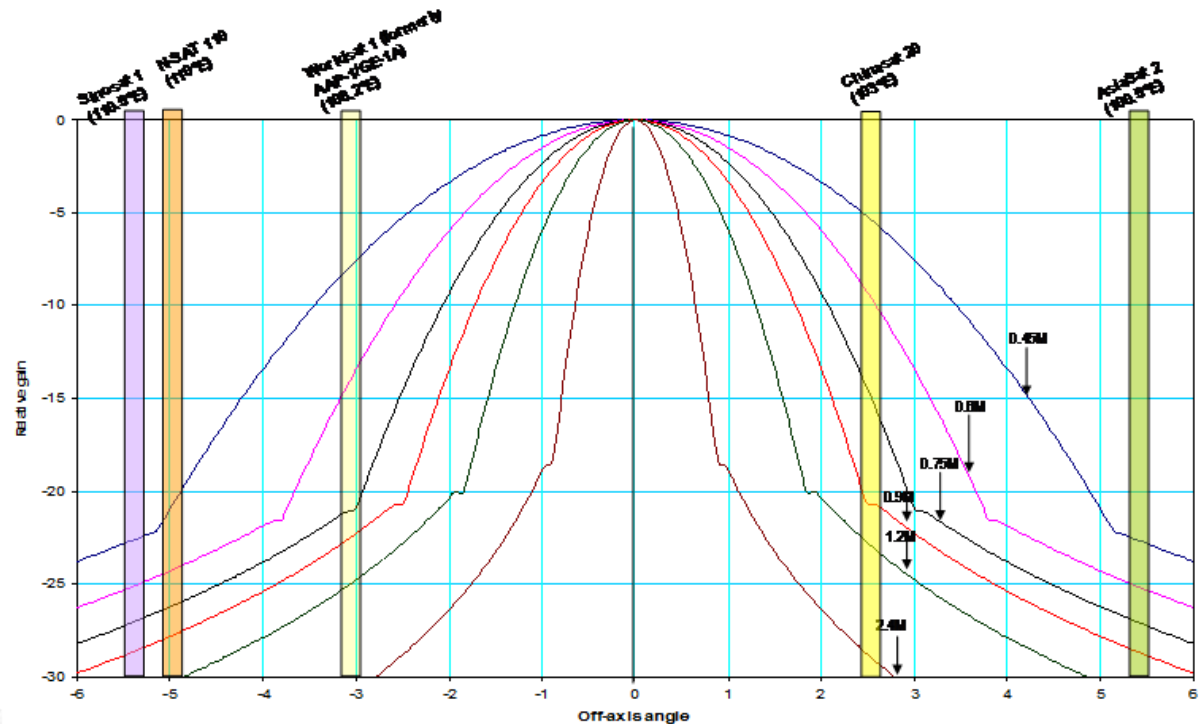
Basic configuration of a LNC

Adjacent Satellites

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❖ Adjacent satellite interference

- Interfered by adjacent satellite operating of co-frequency band and co-service coverage
- Larger antenna, narrower beam width, lower interference
- Figure shows antenna size relative to Ku D/L interference
 - ⇒ beam width for 0.45, 0.6, 0.75, 0.9, 1.2 and 2.4 m antennas



❖ Not good at marketing

- Uncommon frequency band, rarer and more expensive antennas and RF equipments
 - ⇒ allowance often used for customer carriers' migration
- More difficult in transponder rent and sell
 - ⇒ more competitive rent fee often offered

❖ Good at adjacent satellite interference

- Uncommon frequency band, rarer and less interference from adjacent satellite
 - ⇒ easier for frequency coordination
 - ⇒ smaller antenna may be used for market development

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Transponder Resource

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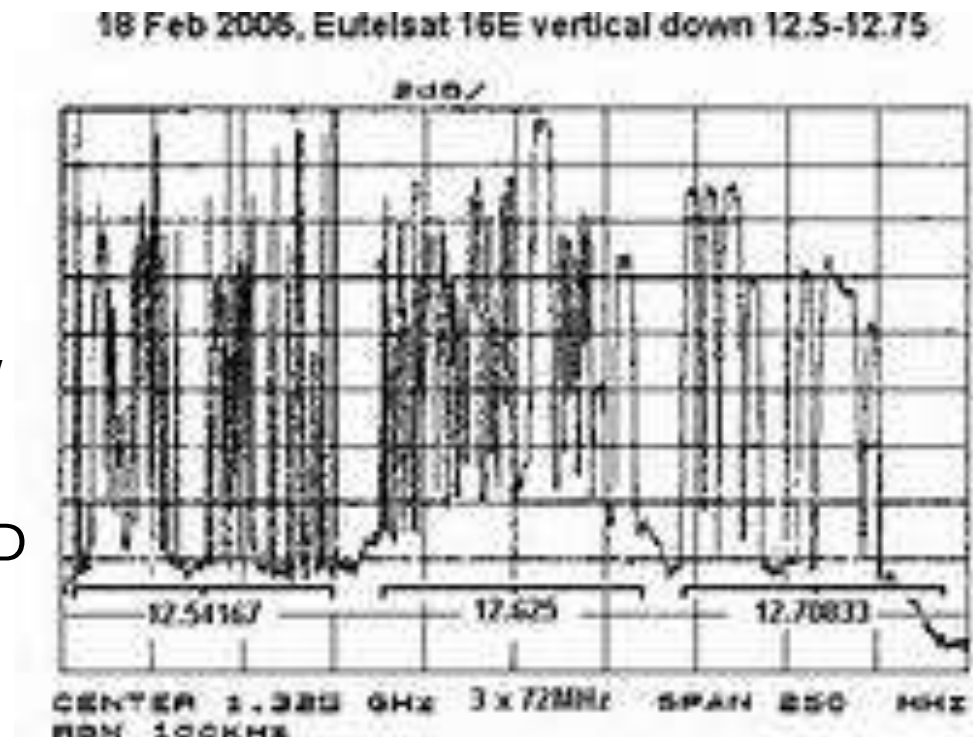
❖ Transponder resource

- Power resource
 - ⇒ EIRP, linear EIRP
- Frequency resource
 - ⇒ bandwidth
- Resource allocation
 - ⇒ sharing EIRP and B/W

❖ Transponder spectrum

- Noise floor showing SFD sensitivity
- Y-axis: EIRP density, dBW/Hz
- X-axis: bandwidth, Hz
- Area: EIRP

$$\text{EIRP (dBW)} = \text{EIRP density (dBW/Hz)} \times \text{bandwidth (Hz)}$$



Transponder Spectrum

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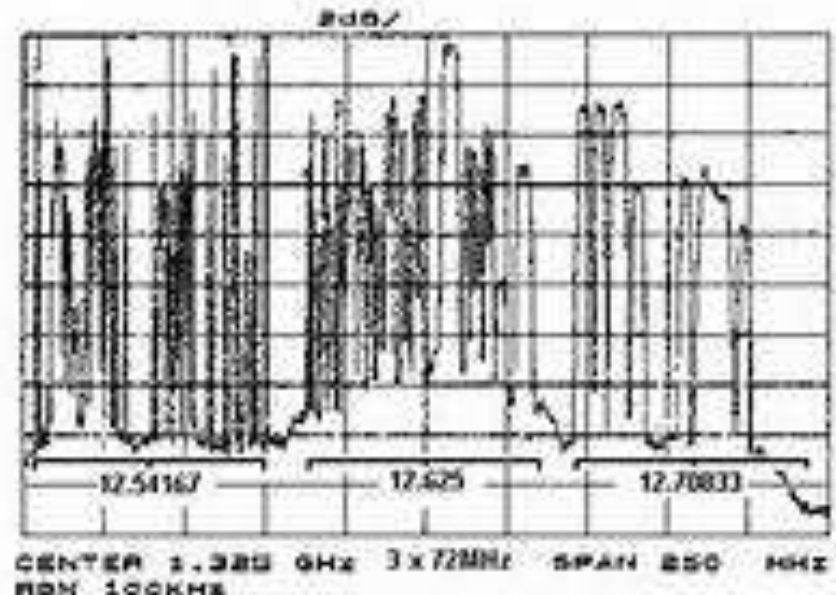
❖ Carriers in transponders

- Higher in Y-axis, higher power density occupied
- Wider in X-axis, more frequency bandwidth occupied
- Larger in area, more power occupied
- Total area of carriers or carrier areas' integral: transponder power occupied by all carriers

❖ Rule of resource allocation

- Keeping carriers as same power density as possible
- More power occupied, more expense offered

18 Feb 2005, Eutelsat 15E vertical down 12.5-12.75



Carrier Spectrum

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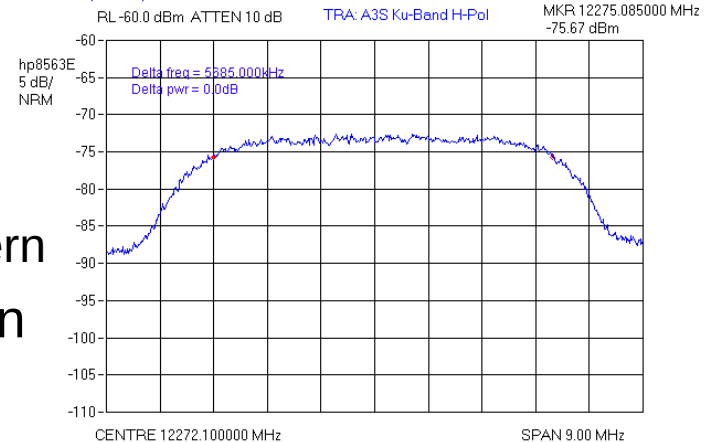
❖ Carriers at spectrum analyzer

- SCPC carrier by phase modulation
 - ⇒ spectrum line at rectangular shape
- TDMA carrier by phase modulation
 - ⇒ spectrum lines as rectangular pattern
- Analog TV carrier by FM modulation
 - ⇒ spectrum lines as pyramid pattern

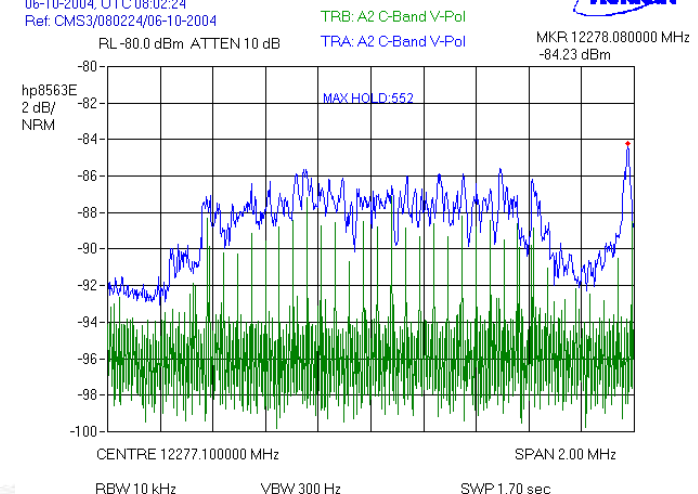
❖ Carrier resource allocation

- Enough frequency bandwidth including guard band
- Average power (density) with clear and flat noise floor

Asia Satellite Telecommunications Co. Ltd.
Carrier Monitoring System
06-10-2004, UTC 06:21:34
Ref: CMS3/062134/06-10-2004



Asia Satellite Telecommunications Co. Ltd.
Carrier Monitoring System
06-10-2004, UTC 08:02:24
Ref: CMS3/080224/06-10-2004



❖ Linearity requirement

- 3rd intermodulation product, noise power ratio, phase shift, and AM/PM transfer
- Better specification at the band around center of transponder

❖ Frequency response

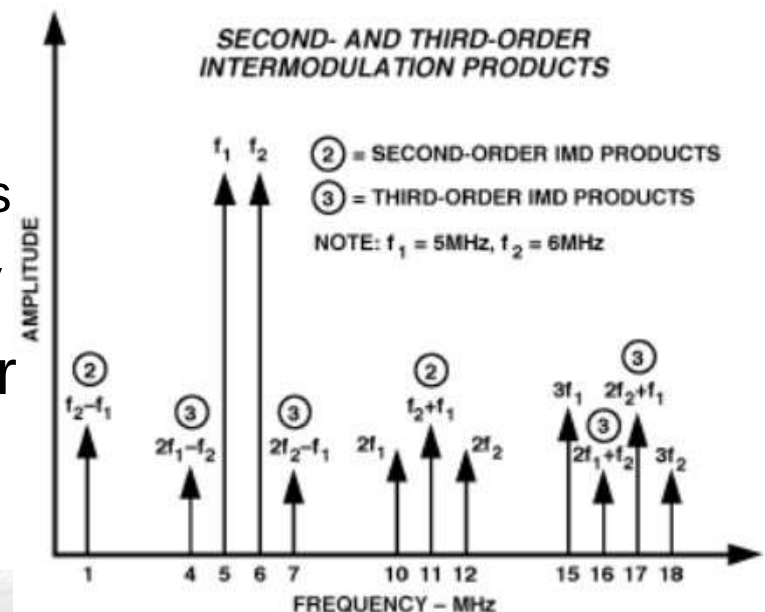
- frequency response, gain slope, and group delay
- Better specification at the band around center of transponder

❖ Cross polarization

- Occurred by polarization adjustment for transmit antennas

❖ Frequency and power stability

❖ Center in transponder is better



Carrier Allocation

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❖ Multi carrier used transponder

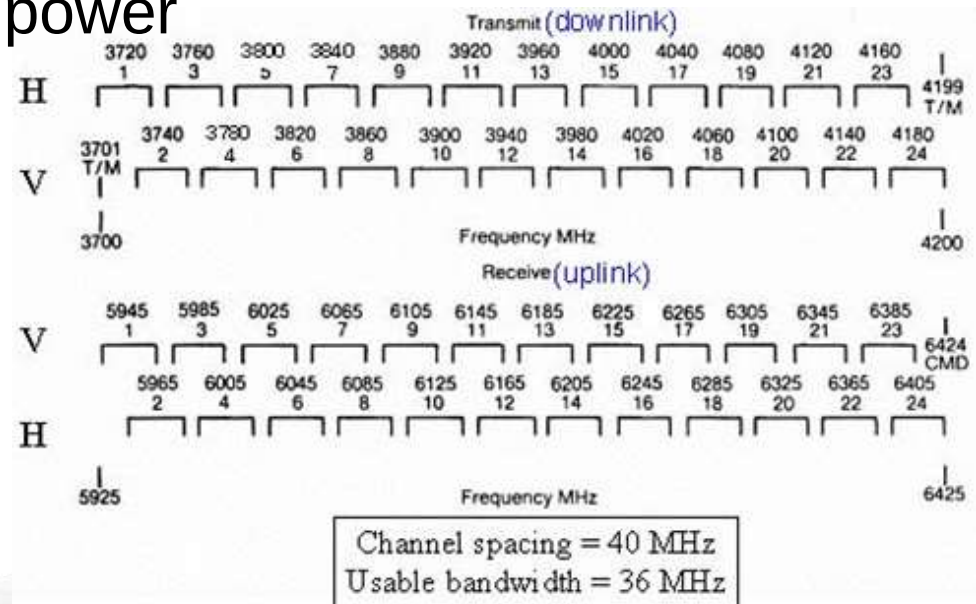
- Center bandwidth properly reserved for pure carrier test
 - ⇒ causing corsspol interference to the transponder at crosspol
- Interleaving frequency plan is better

❖ Center frequency band allocation

- Center is better for carriers easily influenced by non-linearity or phase noise (TDMA and others)

❖ Carriers needed more power

- Asides is better to let IM products going out of band



❖ C-band

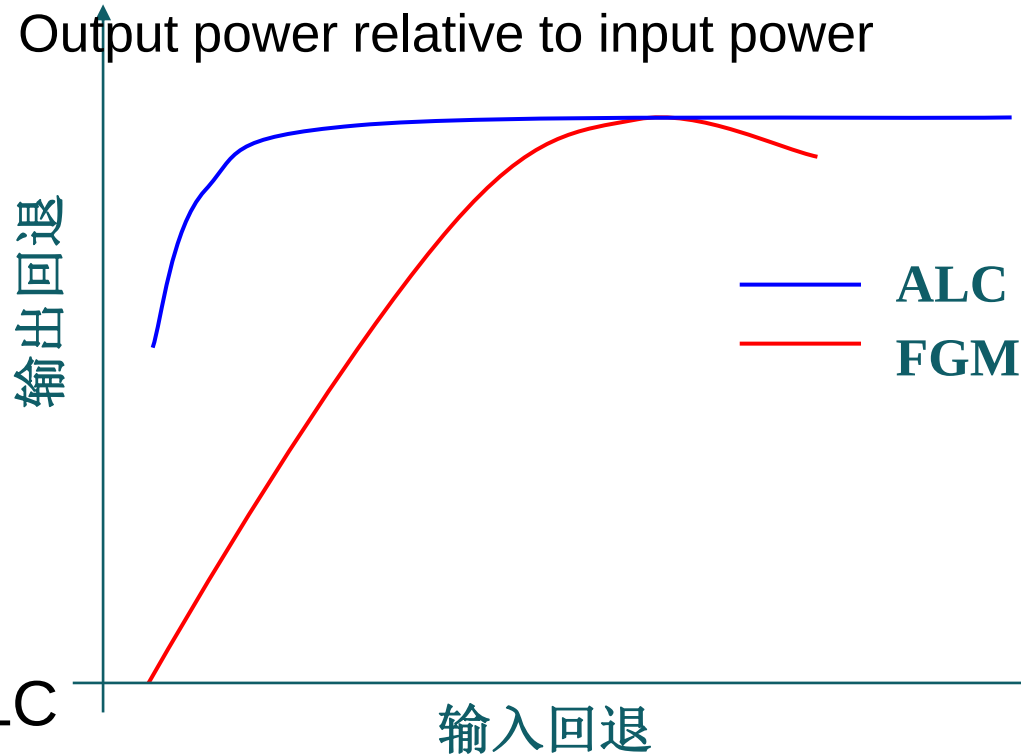
- Larger service area
- EIRP at 36 to 42 dBW, and G/T at -5 to +1 dB/k
- 1.8m or larger antenna for VSAT terminal
- Less climatic influence
- Compliant for high reliability as well as inter continent service

❖ Ku-band

- Smaller coverage
- EIRP at 44 to 56 dBW, and G/T at -2 to +8 dB/k
- 1m or smaller antenna for TVRO and internet access
- Rain fade and other climatic influence
- Compliant for domestic network of numerous terminals

❖ FGM

- Fixed Gain Mode
- Output power relative to input power



❖ ALC

- Automatic Level Control
- Fixed output power at proper input power range
- Suit for broadcast carrier uplinked by single E/S

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❖ Link budget

- One link budget table covering whole transponder bandwidth
- Carriers or carrier groups listed one by one
- Carrier's center-frequency/bandwidth and carrier group's start/stop-frequency/bandwidth with their power level
- Two down-link C/N, one for user's E/S and the other for carrier monitoring at SCC

❖ Carrier spectrum archive

- New plotted spectrum and its noise floor at line-up test
- Regular profiling and comparing

❖ Carrier information and spectrum plots

- Information about carrier and user
- Spectrum plots of the carrier, including neighbouring carriers, and whole transponder

❖ Daily monitoring

- Raised noise pulse or noise floor
 - ⇒ checking transponder and carrier spectrum by wide band and narrow span
- Raised carrier power or intrusive carrier
- Anomaly recording and analyzing
 - ⇒ informing the user and resolving the problem

❖ Interferences in satellite networks

- Often happened
- Hard to find the source
 - ⇒ because of wide coverage, open access, lots of uplinkers, stealers and intruders

❖ Interfering source

- Technical caused
 - ⇒ equipment problem and incorrect operation, accounted for 90%
- Unauthorized uplink
- Intentional intrusion
 - ⇒ economical or political reason

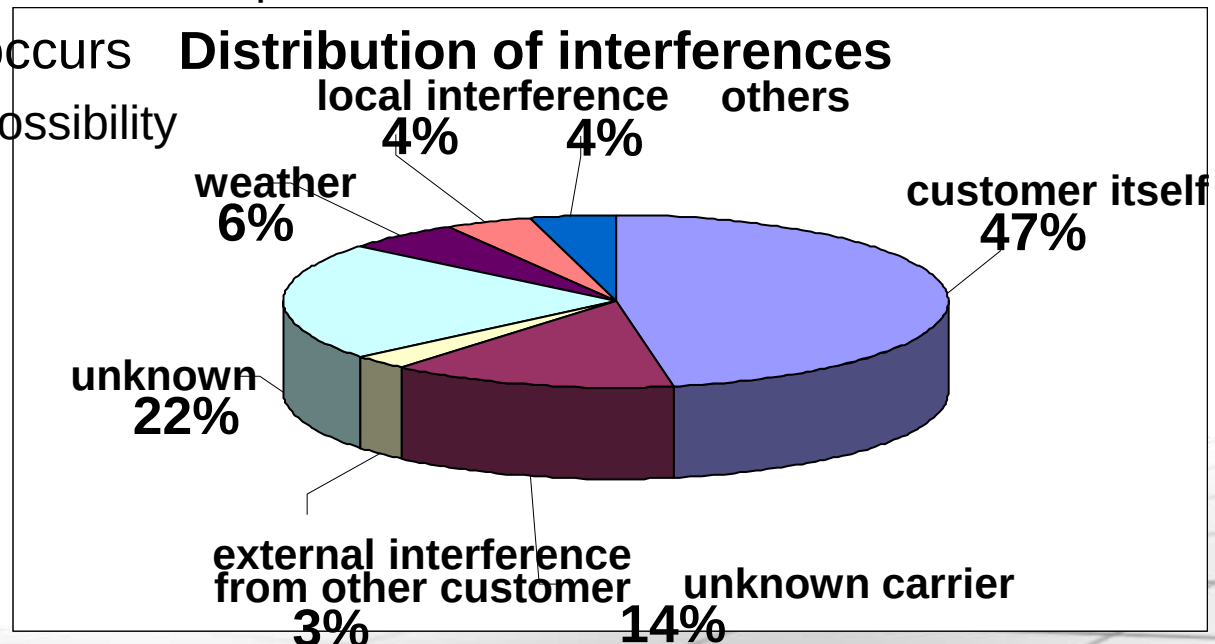
Interfering Measures (cont.)

❖ Classification statistics

- Most of the interferences are caused by improper operation

❖ Measures

- Power level decreased
 - ⇒ U/L problem? Rain fade? Antenna mispointing?
- Noise floor risen
 - ⇒ Intermodulation? Crosspol interference?
- Interference occurs
 - ⇒ too much possibility



❖ Measures of operator's

- Rigorous network management
 - ⇒ equipment verification test
 - ⇒ carrier line-up test
 - ⇒ carrier monitoring system
- Completed interfering coordination
- Enough margin remained at link budget

❖ Measures of user's

- Notice operator before network changed
- Carrier test plan prearrangement with operator

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Frequency Coordination

❖ For potential customers

- Analyzing user's requirement
- Offering link budget based link or network suggestion
 - ⇒ frequency band
 - ⇒ antenna size and HPA power
- Coordination
 - ⇒ user asked antenna size vs. interference coordination requirements
 - ⇒ user asked power vs. power/bandwidth balance
 - ⇒ user asked carrier bandwidth vs. physical truth + guard band

❖ For potential migration customers

- Introducing the advantage of space segment
 - ⇒ less adjacent satellite inference at unique frequency band
 - ⇒ local service, quick response and omnibearing support
- Measuring the difficulty of migration
 - ⇒ unique frequency band for antenna and RF equipments, etc.
- Discussing the process of migration
 - ⇒ working quantity evaluation and migration schedule drafting
- Cooperation
 - ⇒ antenna pointing and pol-angle adjustment
 - ⇒ line-up test for uplink carriers
 - ⇒ other cooperation works

❖ Annual session

- Cooperation with marketing department
- Invitation to all customers
- Transponder resource introduction
- Operating condition introduction
- Common concern discussion
- Technical training

❖ Other technical support

- Cooperation with marketing department

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❖ Verification test

➤ Antenna

- ⇒ side lobe test
- ⇒ crosspol isolation test

➤ RF equipments

- ⇒ spurious, modulation and intermodulation characteristics
- ⇒ power and frequency stability

❖ Line-up test

➤ Antenna

- ⇒ pointing and pol-angle adjustment

➤ Carrier

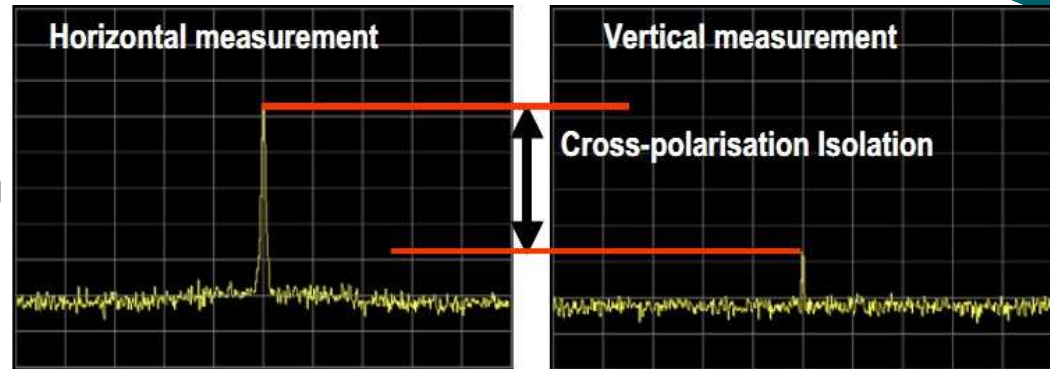
- ⇒ frequency and power calibration

Crosspol Isolation Test

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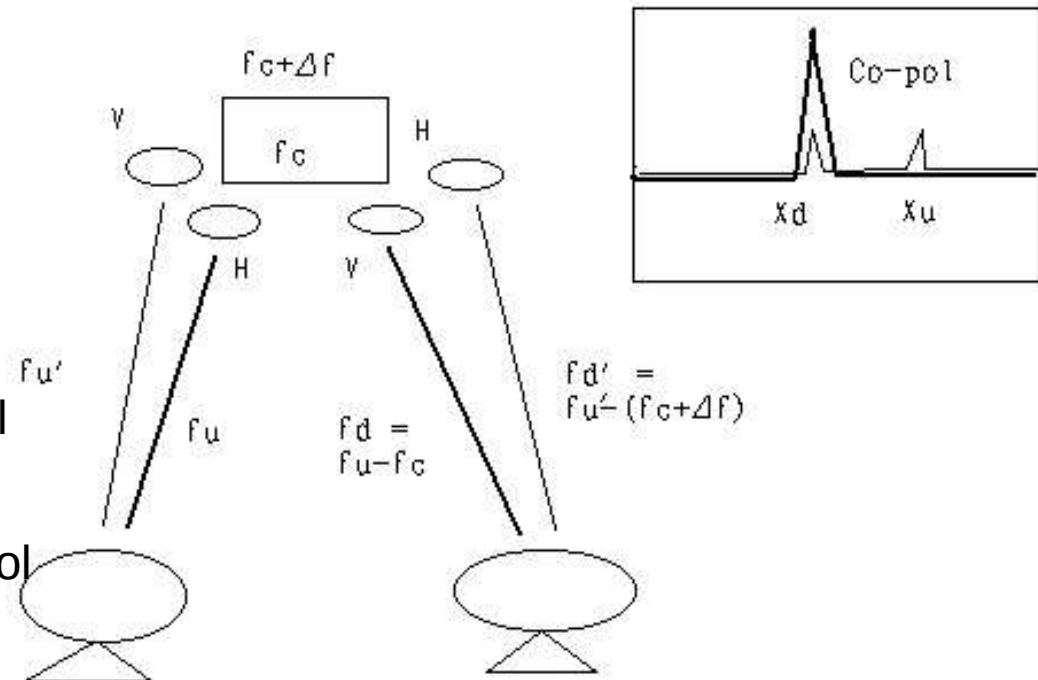
❖ Crosspol isolation

- Power difference at co-pol and X-pol
- Intrinsic specification of antennas
- Better or worse by adjustment



❖ Method

- Change at Tx side
 - ⇒ transmitting at both polarization
 - ⇒ monitoring at co-pol
- Change at Rx side
 - ⇒ transmitting at co-pol
 - ⇒ monitoring at both polarization



❖ Regular customer visiting

- Operating condition review for user equipments
- User claim and requirement listening
- User's future plan discussion
- Service and interference problem suggestion

❖ Customer test cooperation

- Offering idle space segment
- Witness and cooperation for the test
- To avoid unnecessary intrusion, test resource about short term and limited band may be offered for non-user

Adjacent Satellite Interference

❖ Half power antenna beam width

- Beam width at antenna main lobe where -3dB roll off from peak

$$\theta_{3dB} = 70 \lambda/D$$

where, D is antenna aperture, and λ is the wave length relative to carrier frequency

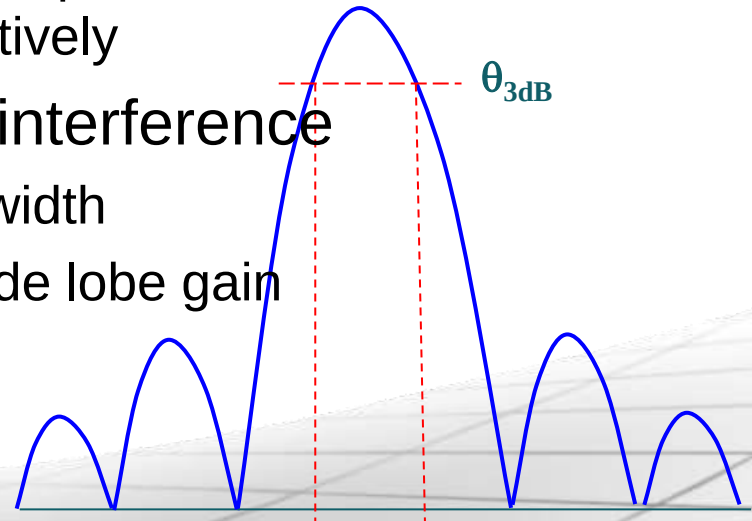
- Antenna could be estimated by beam width

$$G_{ANT} = 31000 / (\theta_{Az3dB} \theta_{El3dB})$$

where, θ_{Az3dB} and θ_{El3dB} are half power beam widths at azimuth and elevation respectively

❖ To decrease adjacent satellite interference

- Larger antenna, narrower beam width
- Wider orbital separation, lower side lobe gain



Adjacent Satellite Interference (cont.)

❖ Down-link interference

- Emission from adjacent satellite received by side lobe of local antenna

$$C/I = (EIRP + G_{RX}) - (eirp + G')$$

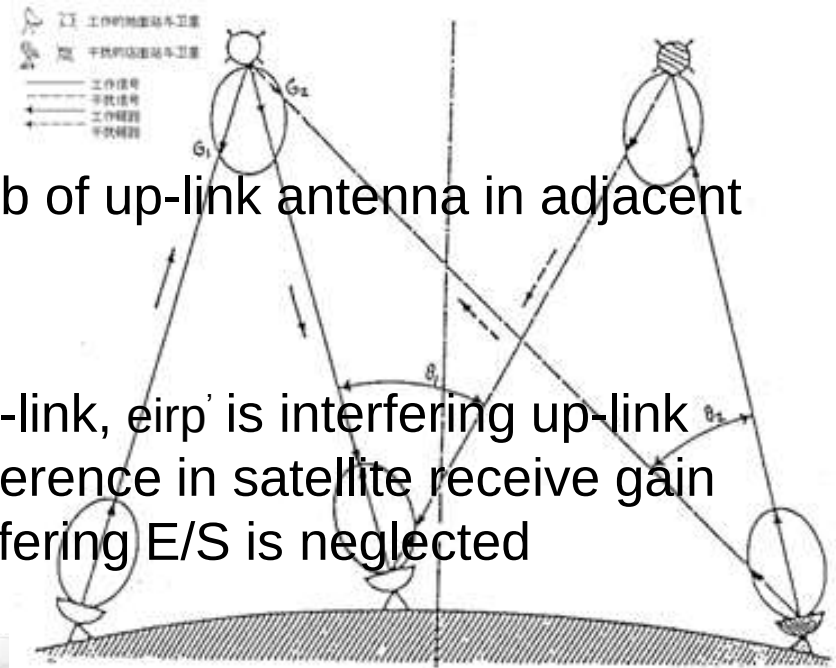
where, C/I is carrier to interference power ratio, EIRP and eirp is wanted and interfering satellite EIRP, G_{RX} and G' is peak antenna gain pointing to wanted satellite and off-axis gain to interfering satellite

❖ Up-link interference

- Off-axis emission from side lobe of up-link antenna in adjacent satellite network

$$C/I = EIRP - eirp'$$

where, EIRP is wanted up-link, eirp' is interfering up-link through side lobe, and difference in satellite receive gain between wanted and interfering E/S is neglected



❖ Cross-polarization

- Closer to beam center, better crosspol isolation
 - ⇒ antenna mispointing causing worse X-pol isolation
- Gain variation by pol-angle changing is more sensitive at X-pol than co-pol
 - ⇒ monitoring X-pol when polarization angle adjustment

❖ Intermodulation

- Unauthorized carrier power increasement
 - ⇒ carrier uplink power may be increased by one user after another, when some of them without regard to allocated power level
- Up-link power losing lock at RF equipment
- Less margin in power allocation

Interference from Earth Station

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- ❖ Unwanted loop formed at RF or IF segment
 - Retransmission raising noise floor
 - ⇒ wide band noise floor raised
 - ⇒ switching off suspects' HPA one by one
 - RF equipment
 - ⇒ down-link signal into up-link
 - Cable coupling
 - ⇒ paralleling IF or L-band cable, especially under ground

Interference from Microwave and Intrusion

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❖ Micro-wave relay

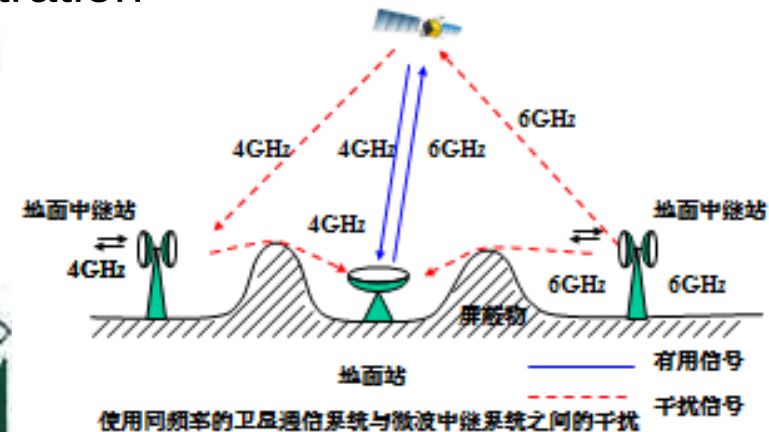
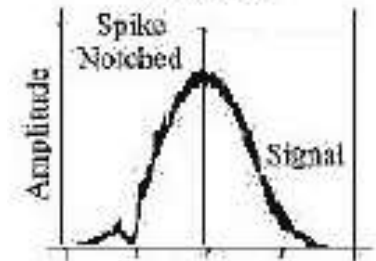
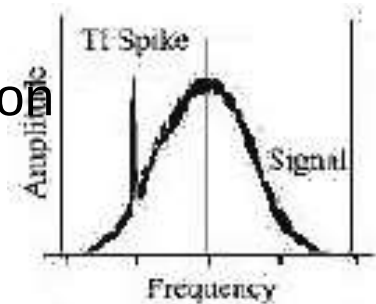
- C-band shared by satellite and terrestrial
- Low elevation angle, parallel to terrestrial emission

❖ Stealing

- Normally for testing in short term
- Improper X-pol adjustment

❖ Intrusion

- Attitude bias for uplink site exploration
- Negotiation with relative administration



- ❖ Absorption of microwave signals by rain
 - Ku-band, up- and down-link
 - 5dB or more attenuation
 - ⇒ with raising noise floor and worse X-pol isolation
 - Insufficient even minus C/N margin
- ❖ Up-link rain fade
 - Uplink power increasing
 - ALC mode presetting for mono uplink transponder
- ❖ Down-link rain fade
 - More margin obligated

Communication Payload

Parameters

Carrier Assignment

Link Budget

Frequency Resource and RF Equipments

Payload Management

Spectrum Assignment

Carrier Management

Technical Support

Marketing Support

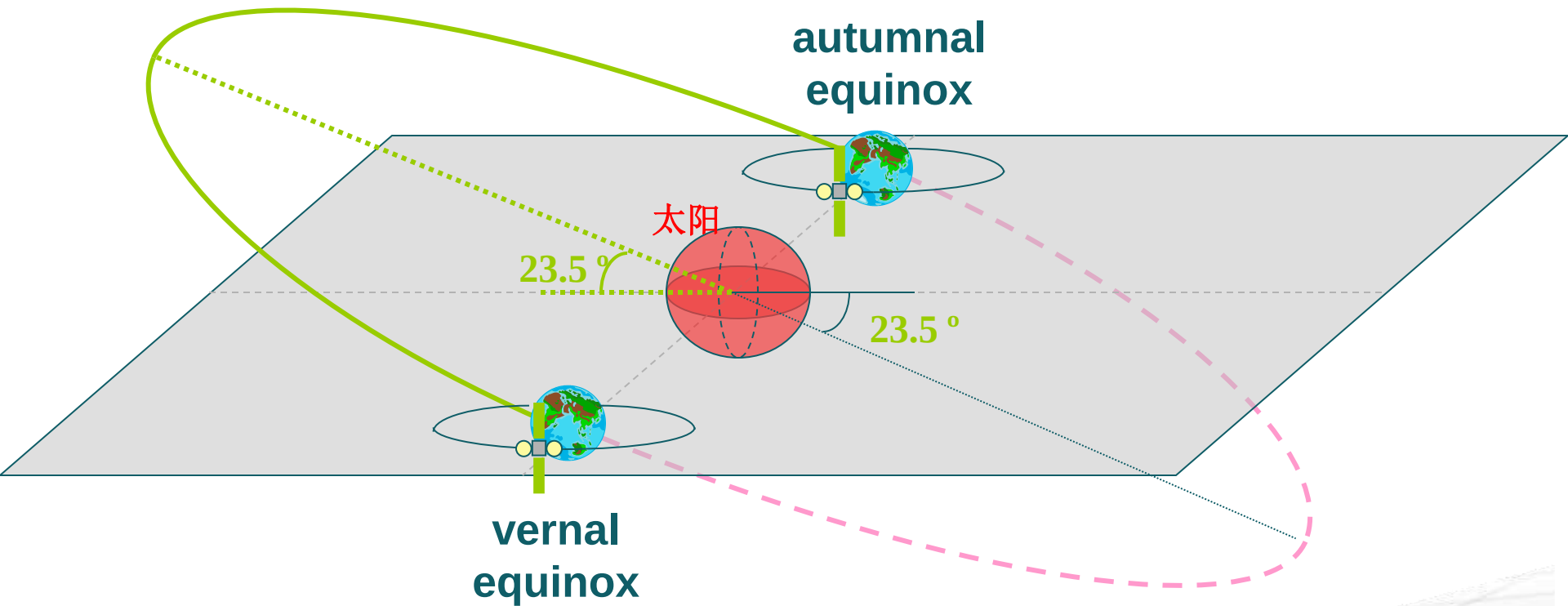
Costumer Support

Sun Outage

Frequency Coordination

Earth Orbit

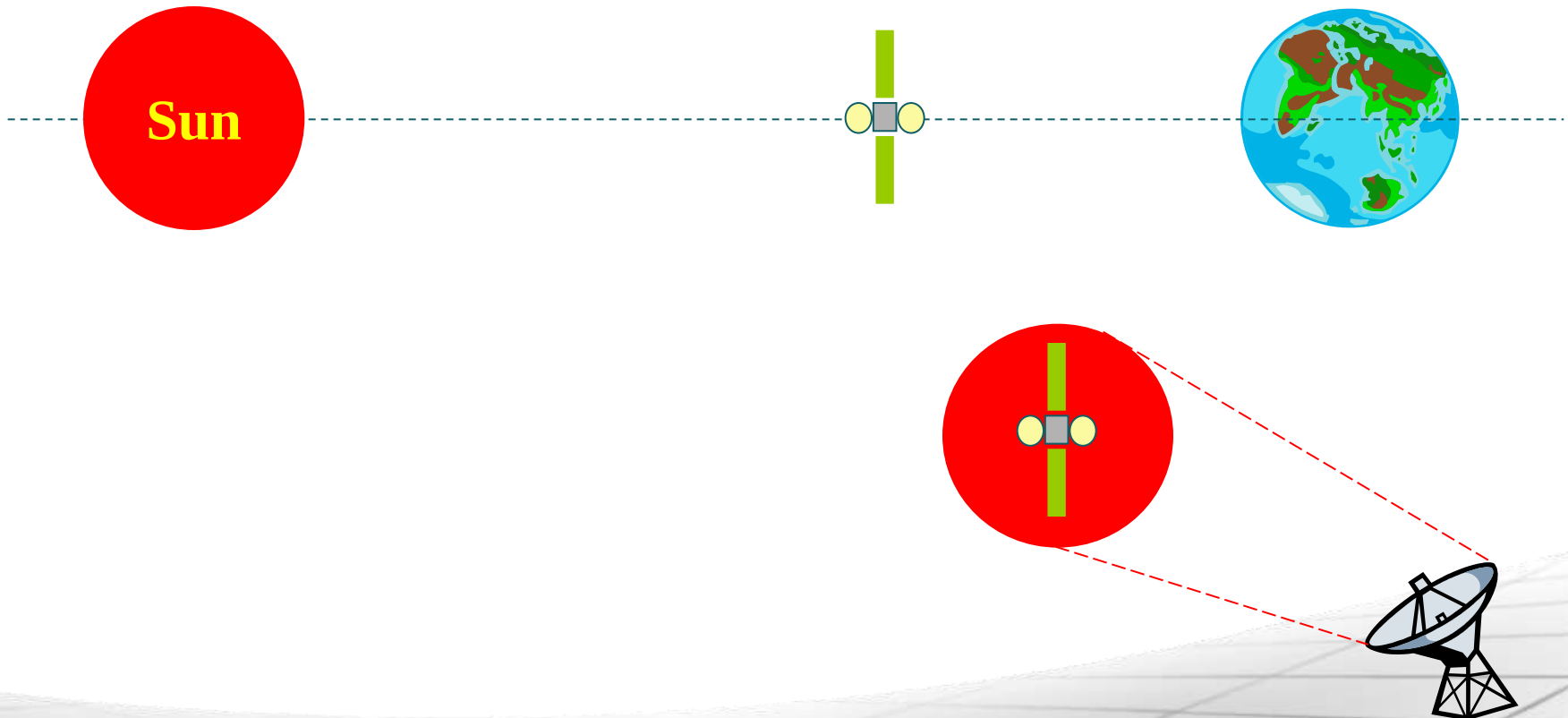
- ❖ Earth orbit is inclined to equatorial plane and GEO
- ❖ During spring and fall equinoxes, the sun passes through the equatorial plane



Sun Outage

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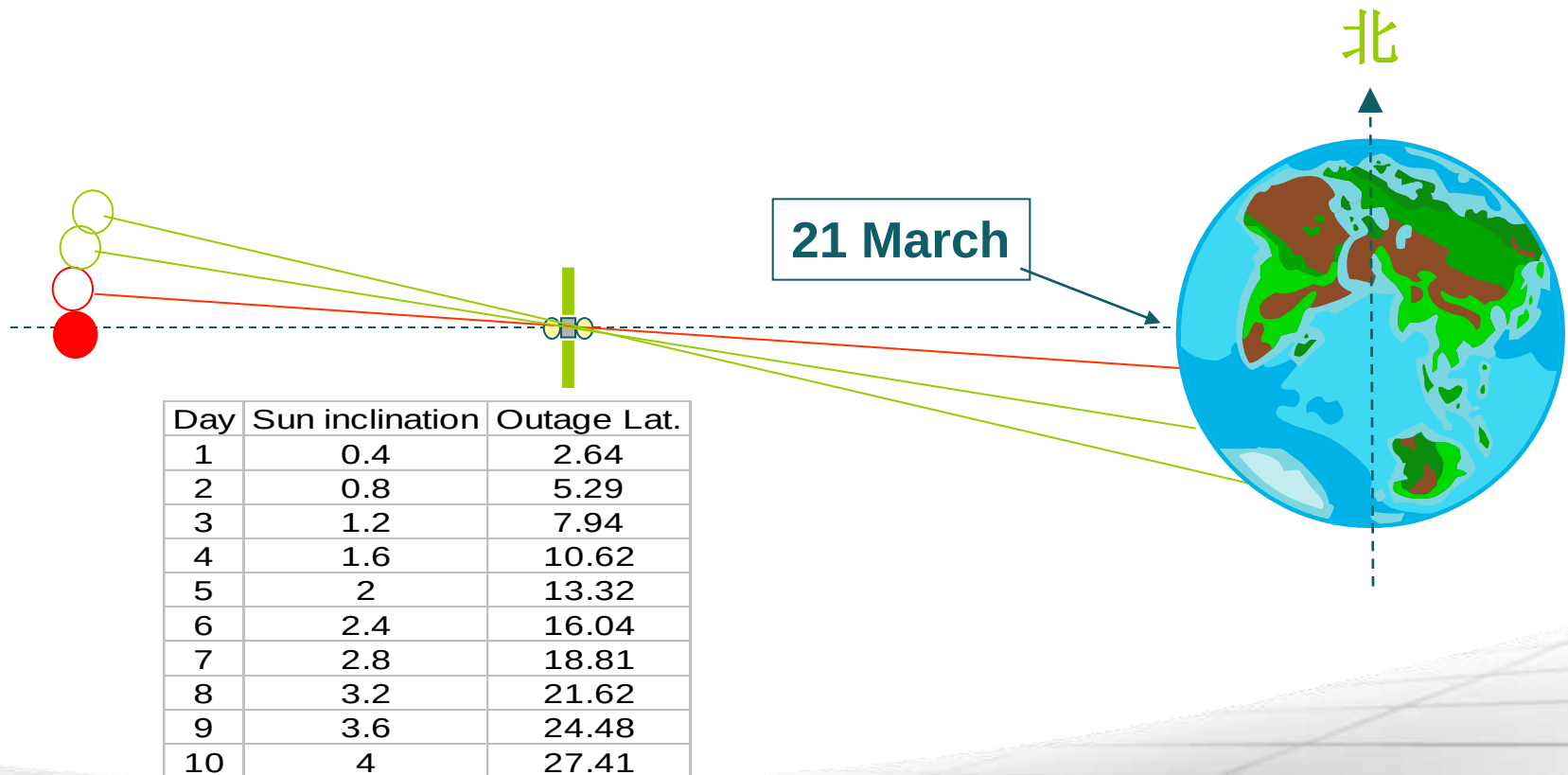
- ❖ When the sun appearing behind the satellite around noon
- ❖ D/L signals from the satellite are overpowered by the RF energy from the sun



Outage date

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- ❖ Solar orbit's daily shift in south/north is 0.4 degrees
- ❖ Outage location's daily shift in north/south is about 2.8 degrees (non linearity)

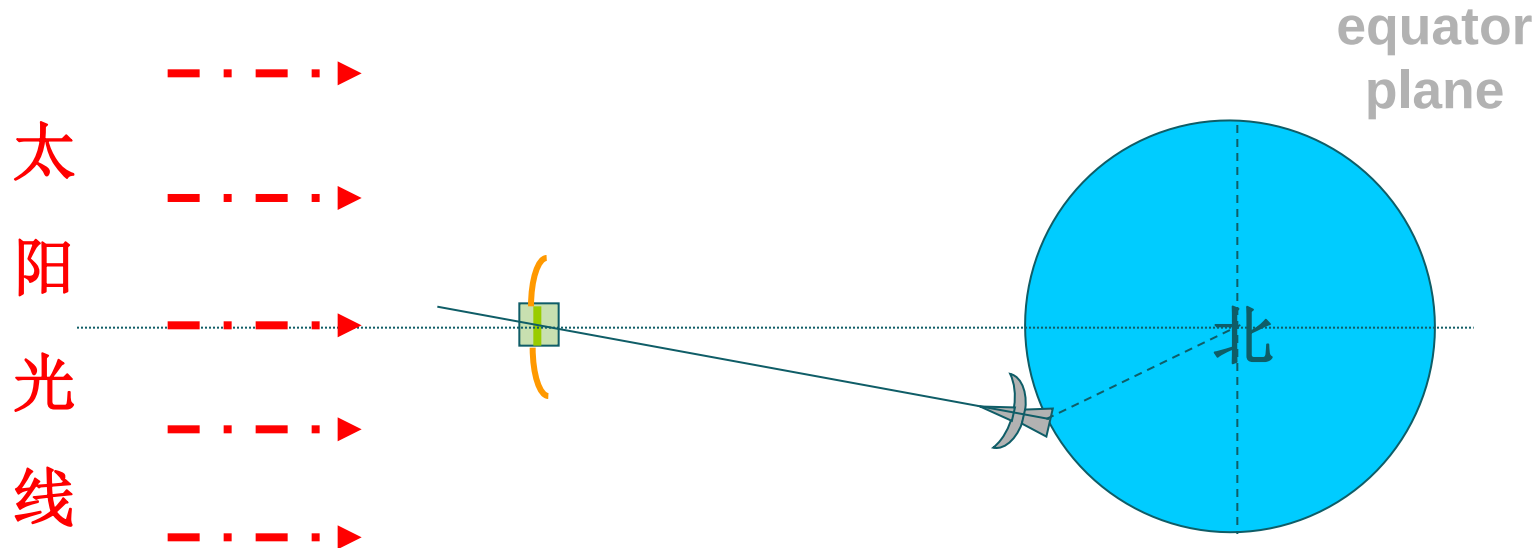


Outage Time

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- ❖ At local noon: E/S longitude equals to satellite orbit
- ❖ Before or after local noon: E/S longitude different to orbit slot

$$\Delta t : \Delta \text{long.} = 4\text{min/deg}$$



Sun Outage Duration

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❖ Outage duration

- Beam width of receiving antenna
 - ⇒ Larger antenna, narrower B/W
 - ⇒ Higher frequency, narrower B/W
- Apparent diameter of the sun
- The difference between noise and signal power
- S/N performance of the receive equipment

天线直径	束宽
2	1.63
3	1.17
4	0.94
5	0.80
6	0.71
9	0.56
11	0.50



❖ Sun outage prediction

- Communication engineer: preparing customer's information
 - ⇒ E/S location, antenna size, and frequency band
- Orbit analyser: calculating outage prediction data
- Communication engineer: sending data
 - ⇒ before each outage period during spring equinox and fall equinox
 - ⇒ to inform customers for preparation

❖ Outage calculator at satellite operator's homepage

- Required input parameters
 - ⇒ E/S location: longitude and latitude in deg, altitude in m
 - ⇒ satellite orbit slot: in deg
 - ⇒ antenna size: in m
 - ⇒ D/L frequency: in GHz

Communication Payload

Parameters

Carrier Assignment

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Carrier Management

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Costumer Support

Sun Outage

Frequency Coordination

Regulation of Frequency Coordination

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❖ Regulation

- Only completed the coordination, could operator use the applied orbital resource
- Standard for coordination: C/I
 - ⇒ coordination for co-coverage and co-frequency band, 10 degrees separation may not meet the requirement
 - ⇒ 2 degrees or more is enough for common operation

❖ Regulation vs. reality

- Relative priority vs. coordination request
- Out-of-date standards vs. technical improvement
- Filing coordination vs. channel by channel discussion
- Face-saving administration vs. hungry so unreasonable operator

❖ C/T

- Carrier power to thermal noise ratio, (dBW/k)
- Internal noise and influence, controlled through link design

❖ C/N

- Carrier to noise power ratio, (dB)

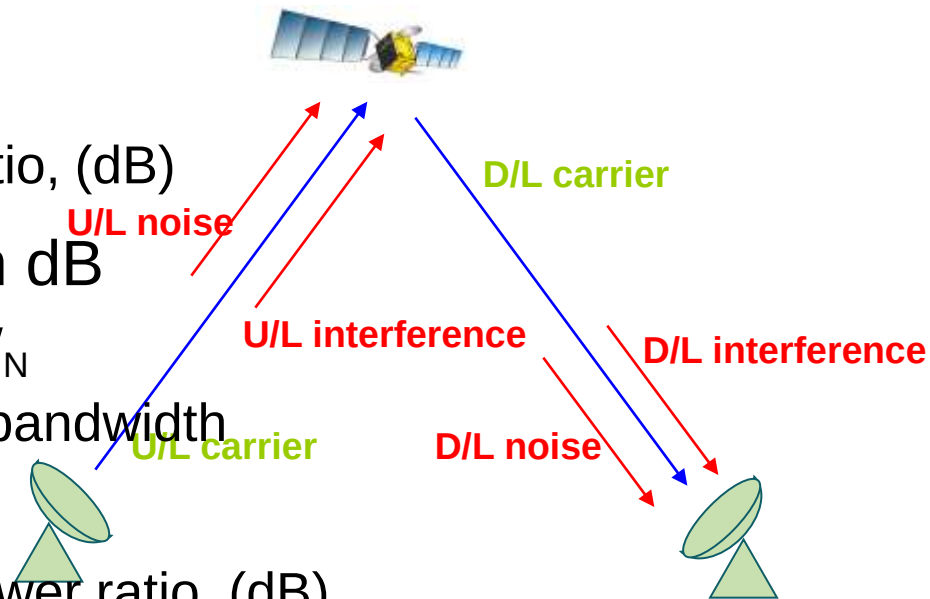
❖ C/T to C/N calculation in dB

$$C/N = C/T + 228.5 - BW_N$$

where, BW_N is noise bandwidth

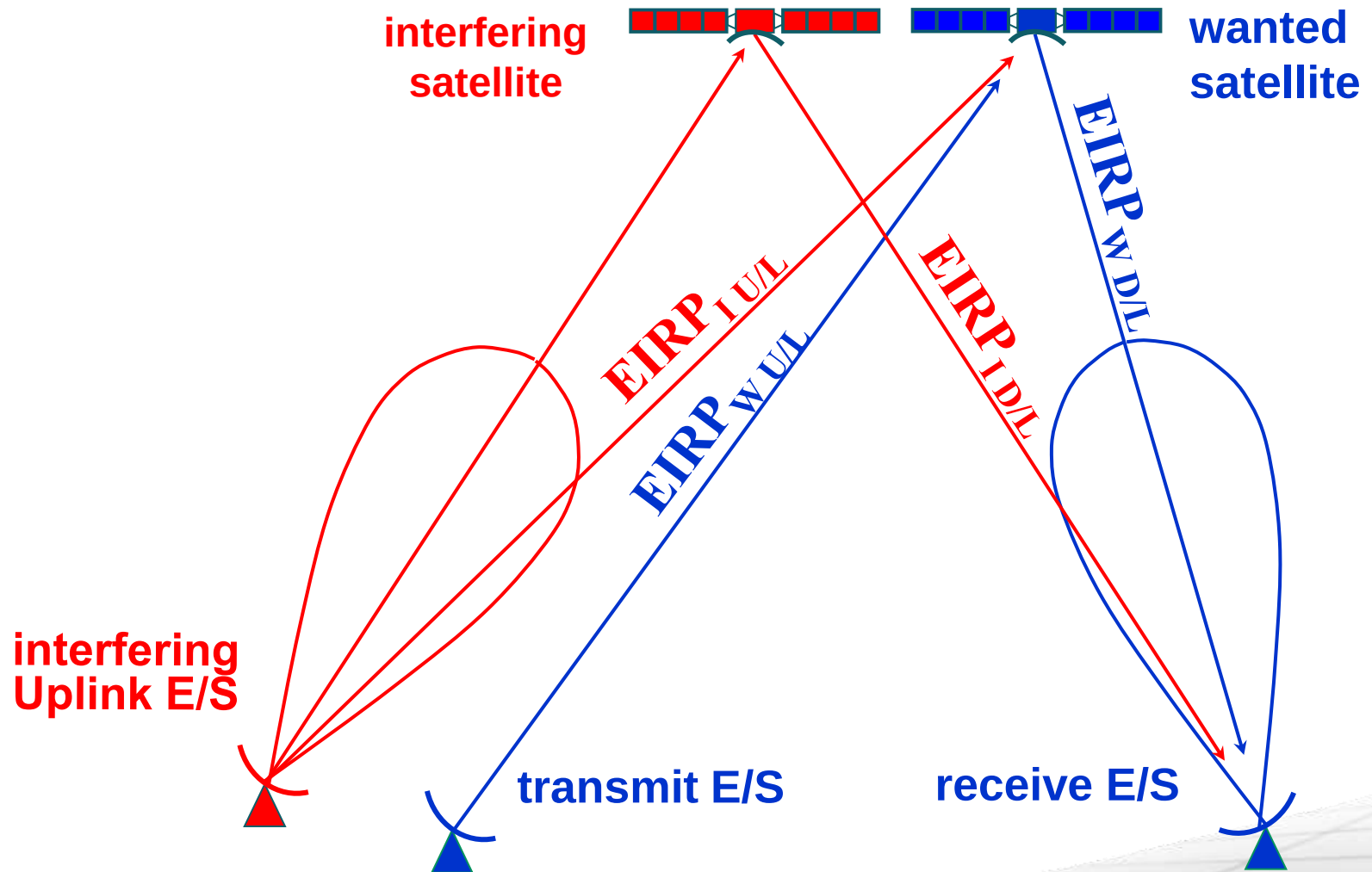
❖ C/I

- Carrier to interference power ratio, (dB)
- By interference power to noise temperature conversion, C/I and C/T can be converted each other



D/L and U/L Adjacent Satellite C/I

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❖ C/(N+I)

- Carrier power to noise and interference power ratio
- Same as thermal noise, interference will also degrade service quality

❖ Relationship between C/T, C/N, C/I, C/(N+I)

$$\left(\frac{C}{I}\right)_U^{-1} = \left(\frac{C}{I_{ACI}}\right)_U^{-1} + \left(\frac{C}{I_{ASI}}\right)_U^{-1} + \left(\frac{C}{I_{XPI}}\right)_U^{-1} + \left(\frac{C}{I_{IM}}\right)_U^{-1} + \dots$$

$$\left(\frac{C}{I}\right)_D^{-1} = \left(\frac{C}{I_{ACI}}\right)_D^{-1} + \left(\frac{C}{I_{ASI}}\right)_D^{-1} + \left(\frac{C}{I_{XPI}}\right)_D^{-1} + \left(\frac{C}{I_{IM}}\right)_D^{-1} + \dots$$

$$\left(\frac{C}{N+I}\right)_U^{-1} = \left(\frac{C}{I}\right)_U^{-1} + \left(\frac{C}{N}\right)_U^{-1}$$

$$\left(\frac{C}{N+I}\right)_D^{-1} = \left(\frac{C}{I}\right)_D^{-1} + \left(\frac{C}{N}\right)_D^{-1}$$

$$\left(\frac{C}{N+I}\right)_T^{-1} = \left(\frac{C}{N+I}\right)_U^{-1} + \left(\frac{C}{N+I}\right)_D^{-1}$$

where, symbol [] means logarithmic notation (dB)

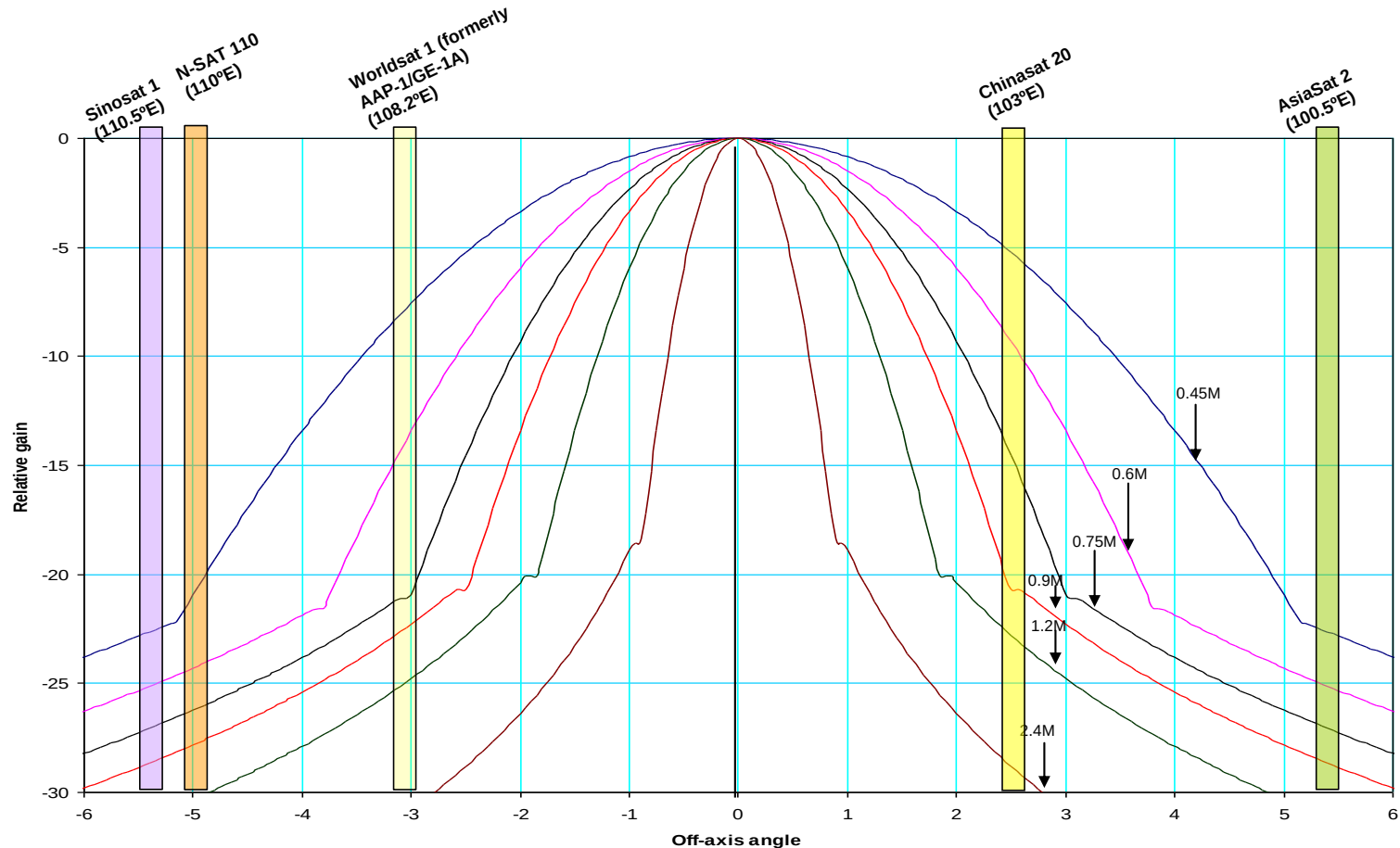
Limited Antenna Size and Power Density

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- ❖ Transponder performance may be limited in use
 - For reducing interference to adjacent satellite, some limitation at antenna size and uplink power density might be committed by the operator
- ❖ System margin may be lower than link budget
 - For uplink interference from adjacent satellite network transmitted by small Tx antenna
 - For downlink interference from adjacent satellite received by small Rx antenna
 - The C/I may be much lower than link budget estimated

Sample of C/I and Antenna Size Relationship

Reception of interference for Ku-band antennas pointing towards AsiaSat 3S (105.5°E)



Relative antenna gain contours for 0.45, 0.6, 0.75, 0.9, 1.2 and 2.4m at 12.2 GHz (ITU-R-BO 1213)

Reference:

AsiaSat: Customer Training Materials, April 2004

Thanks!

Welcome to my homepage

www.satcomengr.com